Unraveling the Correlations between Conformation, Lubrication and Chemical Stability of Bottlebrush Polymers at Interfaces

Jimmy Faivre^{1,3}, Buddha Ratna Shrestha¹, Guojun Xie,² Thierry Delair³, Laurent David³, Krzysztof Matyjaszewski^{2*}, Xavier Banquy^{1*}

¹Canada Research Chair in Bioinspired materials, Faculty of Pharmacy, Université de Montréal, Montréal, Qc, Canada

²Center for Macromolecular Engineering, Department of Chemistry, Carnegie Mellon University, Pittsburgh, PA, USA

³Université de Lyon, Université Claude Bernard Lyon 1, CNRS, Ingénierie des Matériaux Polymères (IMP-UMR 5223), 15 Boulevard Latarjet, 69622 Villeurbanne Cedex, France

Abstract

In the present study, we monitored the conformation and chemical stability of a hydrophilic bottlebrush (BB) polymer in pure water and buffered saline solutions. We correlated these parameters to lubricating and wear protecting properties. Using the Surface Forces Apparatus (SFA), we show that the BB polymer partially adsorbs on mica surfaces and extends half its contour length toward the aqueous media. This conformation gives rise to a strong repulsive interaction force when surfaces bearing BB polymer chains are pressed against each other. Analysis of these repulsive forces demonstrated that the adsorbed polymer chains could be described as end-attached elastic rods. After 2 months of aging at temperatures ranging from 4 to 37 °C, partial scission of the BB polymer's lateral chains was observed by Gel Permeation Chromatography with a half-life time of the polymer of at least two years. The thickness of the BB polymer layer assessed by SFA appeared to quickly decrease with aging time and temperature which was mainly caused by the adsorption to the substrate of the released lateral chains. The gradual loss of the BB polymer lateral chains did not impact significantly the tribological properties of the BB polymer solution nor its wear protection capacity. The friction coefficient between mica surfaces immersed in the BB polymer solution was $\mu = 0.031 \pm 0.002$, and was independent of the aging conditions and remained constant up to an applied pressure P = 15 atm. Altogether, this study demonstrates that besides the gradual loss of lateral chains, the BB polymer is still able to perform adequately as a lubricant and wear protecting agent over a time period suitable for in vivo administration.

Keywords: Bottlebrush polymer, stability, wear protection, polymer conformation

Introduction

Bottlebrush (BB) polymers are composed of a linear macromolecular backbone to which are densely grafted side chains¹. The strong steric repulsion between side chains leads to the backbone extension resulting in a worm-like conformation of the polymer which can be modulated by side-chain grafting density and length^{1, 2}. BB polymers have attracted a growing interest in many application fields ranging from materials to biomedical engineering³. Indeed, grafted or adsorbed BB polymers exhibit exceptional antifouling⁴, viscoelastic⁵, lubrication⁶, surface coating⁷ and photonic⁸ properties. BB polymers combined with contrast agents have also demonstrated exceptional properties as diagnostic tools for MRI and fluorescence imaging⁹. Recent reports are now suggesting the use of BB polymers as drug delivery systems ¹⁰. Contrarily to spherical polymeric particles which have been extensively studied, cylindrical polymer brushes have demonstrated longer blood circulation time^{11, 12} and improved biodistribution¹³, revealing them as promising drug carriers. The BB architecture is abundantly present in nature, in particular in proteins such as mucins and proteoglycans found in articular joints or in the gastro intestinal tract. First reported in natural systems including the protein lubricin 14-19 or agrecans²⁰⁻²² and later in synthetic systems ^{6, 23-27}, the BB architecture is well known to provide excellent friction reduction capabilities to lubricating polymers.

Three main synthetic routes exist to prepare polymeric molecular brushes: the "grafting to" polymerization *via* the coupling reaction of an end-functionalized side-branch to a polymeric backbone; the "grafting through" polymerization of macromonomers bearing the pendant chains and the "grafting from" polymerization of monomers from a macroinitiator³. These techniques can be implemented to grow polymer chains on surfaces or in solution. This allows to obtain a

rich variety of brushes besides the fact that these strategies are challenging to implement due to the steric hindrance between lateral chains and the stress it creates on the BB polymer backbone.

BB polymers chemical stability at surfaces or in solution have been studied extensively 28-30. Different mechanisms leading to BB chemical degradation have been identified. Sheiko et al. reported carbon-carbon bond scissions at the backbone of hydrophobic BB polymers deposited on flat surfaces²⁹. The authors attributed this phenomenon to an increased backbone tension originated by the spreading of the densely grafted side chains on the substrate. Xia et al. observed the same phenomenon with ultrahigh molecular weight cyclic BB polymer deposited on graphite³⁰. Chen et al. reported that end-grafted polystyrene (PS) chains in the brush conformation can also suffer chain scission³¹. The authors explained their results invoking intermolecular transfer reactions which occurred at higher rates for PS brushes compared to free PS chains due to their close packing. Higher degradation rates were also reported for grafted poly(lactic acid) (PLA) brushes compared to bulk PLA³². In this case, the degradation mechanism was mediated by intramolecular transesterification and ester hydrolysis³². Naturally occurring BB macromolecules such as proteoglycans have been reported to undergo degradation as well via proteolysis. This is particularly the case in adult articular joints where the aggrecan, a densely grafted proteoglycan acting as a joint lubricant, suffers from fragmentation by enzymatic chain scission³³. This phenomenon can be accelerated in an inflamed environment such as arthritic articular joints where specific enzymes degrade chondroitin and keratan sulfates glycosaminoglycans side chains.

So far, only a few studies have investigated the changes in BB polymers interfacial properties along with their time-dependent structural changes. In this manuscript, we intent to relate the interfacial properties (normal interaction forces and lubrication forces) of BB polymers to their

chemical stability. We used a BB polymer known to exhibit excellent lubricating properties (friction coefficient $\mu \sim 0.02$) anti-wear properties (pressure at onset of damage > 3 MPa) when combined with high molecular weight hyaluronic acid (HA)³⁴. We first used the surface forces apparatus (SFA) to characterize the interfacial properties of the BB polymer. The wear protection capacity and the lubricating properties of BB polymer solutions as well as the interaction forces between mica surfaces across such solutions were monitored under different aging conditions and correlated to the chemical stability of the polymer. The chemical stability of the BB polymer was assessed by estimating the side chains grafting density using the SFA, the BB backbone contour length by atomic force microscopy (AFM) and the molecular weight of the BB polymer using GPC.

Materials and methods

Polymer synthesis and Formulation. The synthesis of the zwitterionic BB polymer was performed as previously reported³⁴. The polymer was synthesized by atom transfer radical polymerization (ATRP)^{35, 36}, purified by dialysis in pure water prior to recovery. For all stability studies, the BB polymer (white powder) was dissolved at 100 μ g/mL in phosphate buffered saline (PBS, 150 mM NaCl, pH = 7.4) and left in solution in a dark container at 4°C, 22°C or 37°C.

AFM imaging. At different time points, aliquots of BB polymer solutions were diluted with pure water up to a concentration of 50 to 5 μg/mL and deposited on freshly cleaved mica. The BB polymer was left to adsorb for 20 min then exceeding solution was removed using a kimwipe and the surface was washed several times with water to completely remove remaining salt cristals. The surface was air dried prior to imaging. For imaging, a Multimode Dimension 3100 AFM equipped with nanoscope VIII controller (Digital instruments) was used in the peak force QNM mode. Scanasyst-air silicon tips were used for imaging. The contour length of the BB polymer was obtained by analysing AFM images using WormTracker plug-in for ImageJ³⁷.

Interaction forces. A Surface Forces Apparatus (SFA 2000, SurForce LLC, USA) was used to measure the interaction force profiles between mica surfaces across BB solutions. Briefly, back-silvered mica sheets were glued (epoxy glue Epon 1004F) on glass cylindrical disks with a curvature, R, of 2 cm under a laminar flow hood. The disks were then mounted in the SFA chamber in a cross configuration. The SFA chamber was then purged with dry argon and the surfaces were brought into adhesive contact to quantify the mica surfaces' thickness. The surfaces were then separated again and 50 μ L of BB polymer solution were injected between the

surfaces. To avoid evaporation of the solution during experiment, pure water was deposited at the bottom of the chamber to saturate the closed atmosphere. The setup was left to equilibrate for 1 h before measurements were started. The separation distance between the two opposing mica surfaces was determined by multiple beam interferometry. The wavelength of the Fringes of Equal Chromatic Order (FECO) was measured with a spectrometer and converted into separation distance using the three layer interferometer model³⁸. The normal interaction forces, F_N , were recorded as a function of separation distance, D, for in (compression) and out (separation) runs at a speed of 1 nm/s. The fringes were analyzed using a in-house Matlab® routine. Experiments were performed at least three times at different contact positions.

Tribological experiments. The friction forces, F_t , as a function of normal force, F_N , were measured using the friction device and bimorph slider³⁹. As in the interaction forces section, 50 μL BB polymer solution were injected between the surfaces and a small amount of pure water was added in the chamber to limit evaporation. The setup was left to equilibrate for 1 h before experimentation. To ensure reproducible BB polymer surface coverage, normal force profiles measurements were carried out right before tribotesting. The normal force was monitored using semi-conductive strain gauges mounted on the double cantilever of the bimorph slider. Friction and normal forces were recorded on a digital recorder (Soltec TA220-2300A). The sliding velocity was fixed at 2.5 μm/s using a Function/Arbitrary waveform generator (Agilent 33250A). The amplitude of the sliding motion was set to 50 μm. The separation distance, D, wear initiation and surface contact area were simultaneously monitored during tribological experiments by continuously recording the FECO using a CCD camera⁴⁰.

Gel Permeation Chromatography (GPC). Monitoring of the molecular weight and dispersity of the BB polymer was assessed by GPC with an eluting phase of 10mM phosphate aqueous

buffer at pH 7.4. The GPC was equipped with a light scattering HELEOS (Wyatt), refractive index detector rEX, Wyatt QELS+ and UV detectors and a PL aquagel OH M 8 micro and H 8 micro columns. The flow rate was set at 0.5mL/min and the system was systematically equilibrated at 25°C for all measurements. The value of the BB polymer refractive index increment, dn/dc, was set to 0.142 mL/g ⁴¹.

Results and discussion

The chemical composition of the BB polymer was (PBiBEM₄₅₉-g-PMPC₃₅)-stat-PMMA₃₇₀ (see figure 1A). A similar polymer was recently shown to have excellent lubricating properties with a friction coefficient close to 10^{-2} under a normal pressure of 15 atm when used in combination with high molecular weight hyaluronic acid in buffered saline.³⁴ These properties make this polymer a promising candidate for biomedical applications such as viscosuplementation of osteoarthritic joints to re-establish wear protection and possibly decelerate cartilage erosion. The architecture of the BB polymer used in this study, shown in figure 1A and B, mimics the lubricating proteins encountered in synovial joints^{6, 42} such as lubricin and aggrecans. The contour length of the BB polymer, measured by AFM imaging, was found to be 141 ± 25 nm. Figure 1C represents a perpendicular cross-sectional profile of the BB polymer deposited on a

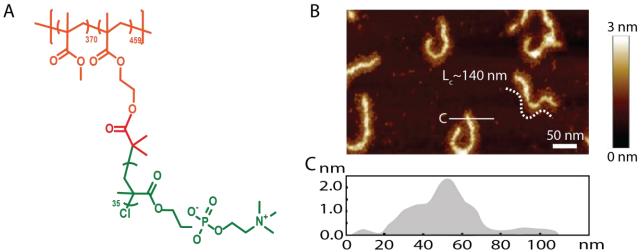


Figure 1. (A) Chemical structure of the bottle-brush polymer used in the study. (B) AFM picture of BB polymer deposited on mica surfaces from a 10 μ g/mL polymer solution. (C) BB height profile of a perpendicular cross-section indicated with the white line in fig. 1B showing the contour of the polymer. mica substrate. The hydrophilic side-

side chains of the polymer appeared to spread on the surface suggesting a favorable affinity towards the surface.

We used the SFA to measure the interaction profiles across BB polymer solutions in water or in saline solutions (Fig. 2A). As can be seen in Fig. 2B, repulsive forces were recorded during the in (surfaces approach) and out (surfaces separate) runs. At a fixed BB polymer concentration of $100 \mu g/mL$, the profiles were identical, independently of the ionic strength of the medium, as previously observed for polyzwitterionic brushes. At a fixed BB polymer concentration forces, given by the separation distance at which adsorbed BB chains facing each other start interacting (D_{onset}) , determined at $F_N/R = 0.01 \text{ mN/m}$, ranged between 125 to 150 nm. The onset of interaction being equal to twice the adsorbed polymer layer thickness, L (L=62-75 nm, no interdigitation hypothesis, see schematic Fig. 2C) and the average contour length of the polymer L_c being equal to $\sim 140 \pm 20 \text{ nm}$ (assessed by AFM), we can conclude that adsorbed BB polymer chains extend on average half their contour length toward the medium. Under high pressure, the BB polymer film is about 5 nm thick, indicating the presence of at least one molecular layer of polymer.

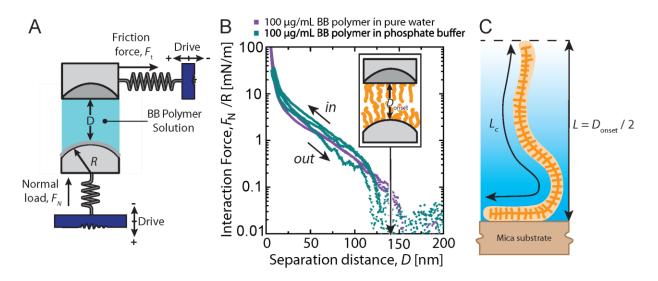


Figure 2. (A) SFA experimental setup used for normal force profiles and tribology experiments. (B) Interaction force profiles across BB solution at $100 \mu g/mL$ in pure water and in a phosphate buffer at

150 mM NaCL and pH 7.4. C) Schematic representation of the BB polymer conformation on the mica substrate with its characteristic dimensions.

In order to determine the conformation and interfacial properties of the polymer, we performed measurements of interaction forces between mica surfaces across solutions of BB polymer at two different concentrations (10 and 100 μ g/mL) and two different saline conditions (pure water and PBS). The measured interaction forces shown in Figure 3A present features common to all tested conditions. The force profiles (F_N/R vs D) were once again purely repulsive even at 10 μ g/mL where the surfaces were not fully covered (Figure 1B) which could have facilitated polymer bridging. Another interesting common feature is the constant onset of interaction forces for all polymer concentrations or saline conditions tested. Such behavior is quite unusual since the conformation, and therefore the polymer layer thickness, of randomly adsorbed or end-grafted linear polymer chains' conformation is known to depend on chain surface density.⁴⁵

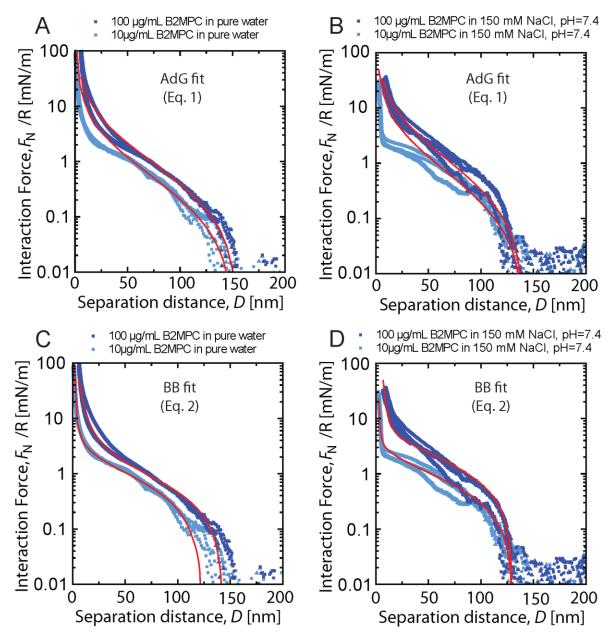


Figure 3. (A) Interaction force profile between mica surfaces across a solution of BB polymer in pure water (A and C) and in buffered saline (B and D). The red lines are the best fitted curves using Eq. 1 (AdG fit) and Eq. 2 (in the manuscript, BB fit).

Reports on interaction forces between BB polymer coated surfaces are scarce, therefore analysis of the present experimental force profiles needs particular attention. In order to analyse the interaction profiles, we used two different theories: the Alexander-de Gennes (AdG) brush

theory⁴⁶ (Eq. 1) and a theory based on the entropy and bending energies of BB polymers (BB model, Eq. 2).

In the AdG brush theory, the interaction energy between two flat surfaces bearing polymer brushes, W, which is related to the interaction force via the Derjaguin approximation ($F_N = 2\pi RW$) has two main contributions: an osmotic contribution that increases as separation distance between the surfaces decreases due to concentration of polymer segments, and an elastic contribution that decreases with the separation distance. The resulting force law reads:

$$\frac{F_N}{R} = \frac{16\pi k_B TL}{35s^3} \left[7 \left(\frac{2L}{D} \right)^{5/4} + 5 \left(\frac{D}{2L} \right)^{7/4} - 12 \right]$$
 (Eq. 1)

where = $1/\sqrt{\pi\Gamma}$.

The AdG model has been shown to apply to many different systems, not only to end grafted brushes. Studies have demonstrated that the AdG model describes correctly the density profile and interaction profiles between end-adsorbed diblock polymers⁴⁷. It also described fairly well the density profile of polymer loops and their interaction forces⁴⁸. Interaction forces between surfaces bearing lubricin followed the AdG model as well.¹⁴ Therefore we can assume that the same model could apply to the present system. The tests performed at different polymer concentrations demonstrated that the AdG model was not able to fit satisfactorily the data in the whole range of concentration studied (Fig. 3A and B). Indeed, from the data provided in Table 1, we can immediately see that AdG model does not fit satisfactorily the experimental data at low polymer concentration. The force profiles also demonstrate that the onset of interaction is insensitive to the polymer solution concentration (and therefore to the surface density as well) which is inconsistent with the AdG brush model. Indeed, the AdG theory predicts that the brush

height L is given by $L \sim N\Gamma^{1/3}$ where N is the number of segments per chain and Γ the grafting density.

Table 1: Brush layer thickness and grafting density obtained from AdG model (Eq. 1)

	PBS			Pure water			
	$\Gamma [\mathrm{nm}]^{-2}$	L [nm]	R^2	Γ [nm] ⁻²	L [nm]	R^2	
10 mg/mL	1.5×10^{-3}	71	0.62	2.2×10^{-3}	77	0.51	
100 mg/mL	$2.1\times10^{\text{-}3}$	70	0.95	3.4×10^{-3}	75	0.94	

Recent simulation studies have proposed that grafted BB polymers behave as elastic rods. ⁴⁹ AFM images confirmed that the persistence length of the polymer adsorbed on mica surfaces was similar to the contour length of the polymer (Figure 1B) therefore supporting this assumption. In this framework, the expected contributions to the total interaction energy between BB polymer coated surfaces are the bending energy of the rod ⁴⁹ and its conformational entropy. ⁵⁰ Considering these two contributions, the interaction forces can be written as:

$$\frac{F_N}{R} \approx A k_B T \frac{\Gamma^2}{D^4} + B k_B T \Gamma \ln \left(\frac{2L}{D}\right)$$
 $D < L$ (Eq. 2)

The first left-hand term in Eq. 2 represents the bending contribution of the BB polymer at the anchoring point (A being a prefactor depending on the brush architecture and Γ the grafting density) ⁴⁹ and the second term, the entropic contribution of the non-adsorbed portion of the BB polymer (L being the height of the BB polymer layer and B being a prefactor close to unity). At low grafting density, Eq. 2 predicts that the entropic contribution is the main contribution to the long range forces. Therefore, under such conditions, the onset of the interaction forces is expected to depend weakly on the grafting density as observed experimentally (see Fig 3). In table 2 we show the fitted parameters using Eq. 2 (parameters for the entropic term only are shown for comparison purposes). As can be seen in figure 3C and D and Table 2, equation 2

shows excellent agreement with the experimental data independently of the ionic strength of the medium or the polymer concentration.

Table 2: Brush layer thickness and grafting density obtained from Eq. 2

	PBS			_	Pure water			
	Γ [nm] ⁻²	<i>L</i> [nm]	R^2		$\Gamma [\mathrm{nm}]^{\text{-}2}$	<i>L</i> [nm]	\mathbb{R}^2	
10 mg/mL	4.2×10^{-2}	65	0.95		4.4×10^{-2}	60	0.91	
100 mg/mL	7.8×10^{-2}	67	0.97		8.0×10^{-2}	67	0.97	

Impact of aging on the BB polymer conformation at interfaces

Using the framework of the rod-like behavior described by Eq. 2, we performed measurements of interactions forces between surfaces across aged BB polymer solutions. In this study, we used PBS as the solution medium and stored the polymer solutions at three different temperatures for a period of several weeks. Figure 4 presents the evolution of the measured interaction forces with the storage time at 4 °C, 22 °C and 37 °C. We can notice a systematic decrease of the onset of interaction, $D_{\text{onset}} = 2L$, with the storage time. The decrease of the onset of interaction increased significantly from low to high storage temperature. At high normal forces, the film thickness remained almost constant at ~ 5nm independently of the storage conditions. As shown in Fig. 4, the force profiles were adequately described by Eq. 2 allowing to determine accurately the BB polymer layer thickness, L, reported in Fig. 5.

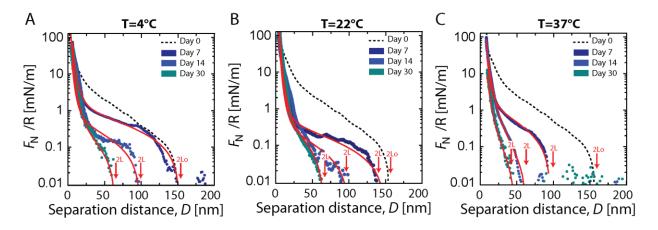


Figure 4. Interaction force profile between mica surfaces across a solution of $100 \,\mu\text{g/mL}$ BB polymer stored during 7, 14 and 30 days in buffered saline at (A) 4°C, (B) 22°C, and (C) 37°C. Dashed line is day 0 BB interaction forces profiles extracted from figure 2.Red lines are fittings obtained from equation 2.

The decay of the onset of interaction L shown in Fig. 5 suggests a gradual change of the BB polymer size or a transition from a rigid to a more flexible BB polymer. Changes in the length of the BB polymer could be the result of a scission of the polymer backbone due to strong steric hindrance generated by the grafted side chains. On the other hand, a transition towards a more flexible BB polymer could be the product of the cleavage of lateral chains over time. Indeed, mean field theory¹ predicts that the mean square size of a BB polymer chain, $\langle R^2 \rangle$, which is, as a first order approximation, related to the onset of interaction L ($L^2 \sim \langle R^2 \rangle$) measured by SFA, is proportional to the side chain grafting density z, i.e. $\langle R^2 \rangle \propto z^\beta$ with β being close to unity. The decay of L^2 (normalized by the onset of interaction at t = 0, L_0) was accurately fitted with a first order kinetic law at all temperatures except 37 °C At this temperature, a second distinct (much slower) kinetic process appears at incubation time longer than 15 days. From these data, the rate constant k of the fast process only was estimated at the different temperatures tested and the corresponding half-life time of the fast process, $t_{1/2}$ was estimated to vary between 10 and 30 days depending on the storage temperature.

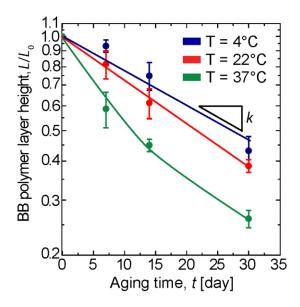


Figure 5. (A) Evolution of BB polymer length using SFA interaction onset and BB fitting as a function of time at 4, 22 and 37°C. Solid lines are guide for the eyes.

In order to confirm the origin of the observed conformational changes of the BB polymers, we first measured the contour length of the BB polymer aged at 22 °C for 60 days by AFM imaging (Fig. 6A). No significant variation in the contour length, L_c , could be observed from the analysis of the AFM images (Fig. 6A and B). Some evidence of side-chains degrafting was obtained by aqueous GPC (in PBS) of the BB polymer solutions stored at different temperatures. The analysis revealed the appearance of a small population of low molecular weight chains at long storage time (peak 2 in Fig. 6C) alongside with a strong and constant peak corresponding to the BB polymer (peak 1). Peak 1 presents a small shoulder that appears at all incubation times and temperatures which was already present in the macroinitiator GPC trace (data not shown). The molecular weight of peak 2 obtained by GPC was close to the expected molecular mass of pMPC lateral chain, $M_w \sim 20~000$ g/mol, and was independent of the storage temperature. This last observation confirmed that degrafting of the lateral chains indeed occurs and happens

predominantly at the junction between the pendant chain and the BB polymer backbone. It could potentially be related to hydrolysis of the ester bonds linking side chains to the backbone. A similar observation was reported for brushes covalently linked to solid wafers in aqueous media. The areas of peak 2 allow to estimate a fraction of degrafted chains of less than 4 % for all tested conditions after two months of storage. These results suggest that the half-life time of the BB polymer is at least 2 years. GPC results can be compared to previous SFA observations. For example, GPC data show a degrafting ratio of 3.5% after one month of aging at 4 °C which corresponds to a grafting ratio z = 0.55 - 0.04 = 0.51. The expected value of the corresponding BB polymer layer L/L_0 is 0.96 which is significantly larger than the value of 0.43 obtained by SFA under the same aging conditions.

The differences between the SFA and GPC kinetic results could originate from small chains released from the BB polymer adsorbing preferentially on the surfaces therefore modifying the affinity / conformation of the BB polymer to the substrate.

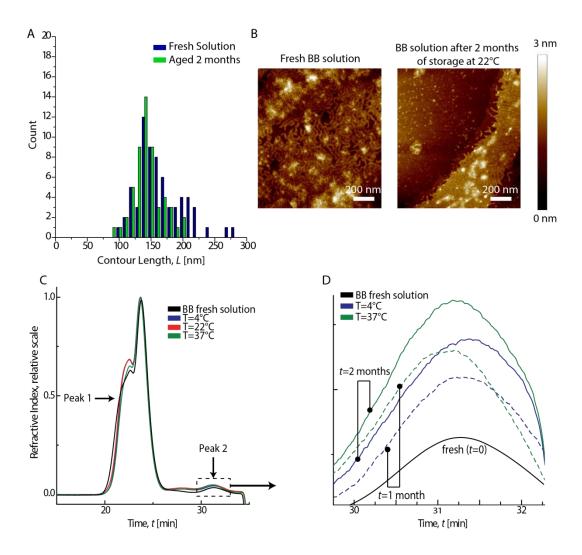


Figure 6. (A) BB polymer contour length distribution in PBS solution at 22°C measured immediately after dissolution and after 2 months of storage analyzed by AFM imaging, (B) Film of BB polymer chains dried on mica immediately after dissolution and after 2 months of storage. A 35 μ g/mL BB polymer solution was used to generate the adsorbed films; (C) GPC traces of aged BB polymer in phosphate buffer, pH = 7.4, at 4, 22 and 37°C compared to a fresh solution; (D) zoom-in of the elution chromatogram of peak 2 region showing the slight increase of the peak with storage time and temperature.

Lubrication and wear protection by aged BB polymers

Finally, we characterized the impact of the structural changes affecting the BB polymer on its frictional properties. Frictional properties of BB polymer fresh saline solution and stored 3 months at different temperatures were recorded using the SFA equipped with a bimorph slider designed for tribotesting. After storage, the solutions were placed in the SFA and friction forces,

 $F_{\rm t}$, were recorded at different applied normal forces $F_{\rm N}$ and constant sliding velocity. As shown in Fig. 7A, a linear relationship between the friction force and the normal force was observed for all samples tested. Such behavior was already reported in a previous report with a BB polymer with a triblock architecture designed to strongly adsorb on the substrate⁶. The linear relationship between $F_{\rm t}$ and $F_{\rm N}$, which is reminiscent of the peculiar rheological properties of the polymer under confinement, allows to extract the friction coefficient (CoF) defined as $\mu = F_{\rm t}/F_{\rm N}$.

The measured CoF of the different solutions of BB polymer before and after the occurrence of damage were $\mu = 0.031 \pm 0.002$ and $\mu = 0.605 \pm 0.040$, respectively (Fig. 7B). Surprisingly, the CoF values before damage were independent of the storage temperature or storage time.

The wear initiation, characterized by the critical pressure of lubricating film rupture, P^* , was obtained through the analysis of the contact shape and separation between the surfaces assessed by multiple beam interferometry³⁸. The measured values were $P^* = 1.49 \pm 0.11$ MPa for BB fresh solution and $P^* = 1.23 \pm 0.16$ for the BB solutions stored 3 months at different temperatures (Fig. 7C).

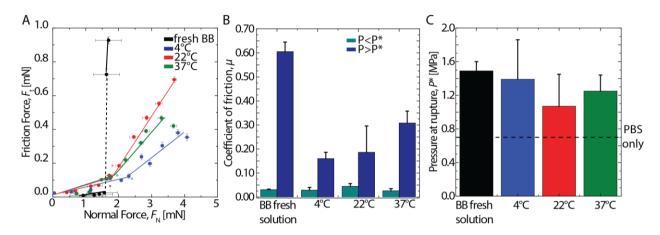


Figure 7. Tribology testing of BB polymer solutions after 3 months of storage in a phosphate buffer, pH 7.4 and 150 mM NaCl, at 4, 22 and 37°C are compared to a BB fresh solution: (A) frictional forces, F_t , as a function of normal force, F_N , (B) Friction coefficient, μ , before (P < P*) and after (P > P*) wear initiation, (C) Evolution of the critical pressure at thin film rupture, P*, hallmark of wear initiation, with the

different storage conditions.

This series of experiments demonstrated that the tribological properties of the BB polymer solution did not present any significant changes after 3 months of storage even if the polymer suffered detectable changes in its structure such as degrafting of lateral chains. We also noticed that the degrafting of the lateral chains of the BB polymer was associated to a less dramatic transition from smooth contact (no damage) to strongly damaged surfaces. A closer look of the evolution of the contact topography, assessed by the FECO shape, revealed that for the fresh BB solution, the wear initiation is not gradual but rather abrupt (Fig 8A a-c and B), due to the sudden formation of aggregates at the edge of the contact (highlighted by a white arrow in figure 8A-c). In contrast, the transition to wear was smoother for aged BB polymer solutions (Fig 8A d-f and B). A gradual accumulation of material inside the contact zone lead to an increase in separation distance before damage of mica occurred. Such smoother transition towards damage can be associated to the presence of degrafted pMPC chains covering the mica surface as previously suggested. The presence of these small and more mobile chains favors the accumulation of material in the contact instead of at the edge.

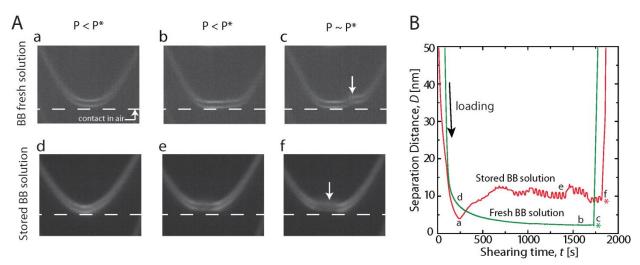


Figure 8. Evolution of FECO fringe shape with pressure for (A) BB polymer fresh solution (a-c), and 3 months aged at 22°C BB polymer solution (d-f) White arrows, in A-c and f, highlight the region of wear

initiation; (B) Separation distance as a function of time for fresh and stored BB polymer solutions. Initiation of wear is indicated by an asterisk.

Conclusions

The present study has shown that BB polymers conformation at surfaces can evolve slowly with time and temperature. Careful experiments with the SFA allowed to quantify the dynamics of such gradual conformational changes and to correlate it with the adsorption of lateral chains on the substrate. These chains were slowly released from the BB polymer via hydrolysis of the linker functional group. The presence of these small chains on the surface did not have any impact on the tribological properties of the BB polymer. We observed no significant difference in the friction of coefficient or the critical pressure at onset of damage between all tested storage conditions. Altogether, the present study demonstrates that the BB polymer is stable enough in PBS to be considered as a potential injectable biolubricant for biomedical applications.

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Author contribution

JF and BRS performed SFA experiments. GX synthesized the polymer. JF and BRS performed tribological work. JF carried out the stability experiments. JF, XB and KM wrote the manuscript.

All the authors participated in the discussion of the data and in the production of the final version of the manuscript.

Competing financial interests:

The authors declare no competing financial interests.

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